

2.2.3.2. Limits of reinforcement ratio

1- Balanced condition (ρ_b)

Ideal condition as when the stress in the steel reaches f_y and stress in concrete reaches max strength at the same time which called balance condition

$$[\sum F_x = 0] C = T ;$$

$$0.85f'_c \beta_1 cb = A_s f_y = \rho_b f_y bd$$

$$\rho_b = \frac{0.85f'_c}{f_y} \beta_1 \left(\frac{\epsilon_{cu}}{\epsilon_{cu} + \epsilon_y} \right)$$

$$\text{Substitute } \epsilon_{cu} = 0.003, \quad \epsilon_y = \frac{f_y}{2.0 \times 10^5}$$

$$\rho_b = \frac{0.85f'_c}{f_y} \beta_1 \left(\frac{600}{600 + f_y} \right)$$

$\rho = \rho_b$: balance, $\rho > \rho_b$: overRC, $\rho < \rho_b$: underRC

2- Maximum reinforcement ratio (ρ_{max})

To make sure that the actual reinforcement ratio $\rho \leq \rho_b$ then the codes limit the reinforcement ratio by maximum ratio of reinforcement

$$\rho_{max} = 0.85\beta_1 \frac{f'_c}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004}$$

If the $\rho > \rho_{max}$ it leads to sudden failure and the section is called over reinforced section.

3- Minimum reinforcement ratio (ρ_{min})

To make sure that the cracks will not appear on the building you must take the reinforcement ratio not less than the minimum value that is:

$$\text{Minimum steel ratio : } \rho_{min} = \max\left(\frac{1.4}{f_y}, \frac{\sqrt{f'_c}}{4f_y}\right) (\text{concrete first crack})$$

$$4 - \rho_t = 0.85\beta_1 \frac{f'_c}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005}$$

2.2.3.3. Reduction Factor (ϕ)





$$\phi = 0.9 \quad \text{if } \rho \leq \rho_t$$

$$\phi = 0.483 + 83.3 \epsilon_t > 0.65 \quad \text{if } \rho > \rho_t$$

$$\text{where } \rho_t = 0.85\beta_1 \frac{f'_c}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005}, \quad \epsilon_t = \epsilon_{cu} * \frac{d_t - c}{c}, \quad \text{and } d_t \approx d$$

2.2.3.4. Design Procedure for Section with Tension Reinforcement only

First step: Select d from the recommended h

				
oneway slab	L/20	L/24	L/28	L/10
BEAM	L/16	L/18.5	L/21	L/8

where $d = h - \text{cover} - \text{stirrup diameter} - 0.5 \text{ main reinforcement diameter}$ Then
Second step: Find b where ($d / b \approx 1.5$ to 2)

Third step: Find W_u

$$W_u = 1.2 \text{ D.L} + 1.6 \text{ L.L}$$

Fourth step: Find M_u as followed:

Case	Positive moment
At end span with discontinuous unrestrained end	$W_u L^2 / 11$
At end span with discontinuous integral with support end	$W_u L^2 / 14$
At interior span	$W_u L^2 / 16$
Case	Negative moment
At exterior face of first interior support for two spans	$W_u L^2 / 9$
At exterior face of first interior support for more than two spans	$W_u L^2 / 10$
At other faces of interior support	$W_u L^2 / 11$

Fifth step: Assume $\varphi = 0.9$ to be check later

Sixth step: Compute tension reinforcement ratio

$$\text{compute } \rho \text{ from: } M_u = \varphi \rho b d^2 f_y \left(1 - 0.59 \rho \frac{f_y}{f'_c} \right)$$

And then check $\rho_{max} \leq \rho \leq \rho_{min}$

$$\rho_{min} = \max \left(\frac{1.4}{f_y}, \frac{\sqrt{f'_c}}{4 f_y} \right)$$

$$\rho_{max} = 0.85 \beta_1 \frac{f'_c}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.004}$$

$$\beta_1 = \begin{cases} 0.85 & \text{if } (f'_c \leq 28 \text{ MPa}) \\ 0.85 - 0.05 \left(\frac{f'_c - 28}{7} \right) & \text{if } (28 < f'_c \leq 56) \\ 0.65 & \text{if } (f'_c > 56 \text{ MPa}) \end{cases}$$

Seventh step: Check φ

if $\rho \leq \rho_t$ then $\varphi = 0.9$

if $\rho > \rho_t$ then $\varphi = 0.483 + 83.3 \epsilon_t > 0.65$
and redesign from step five

where $\rho_t = 0.85\beta_1 \frac{f'_c}{f_y} \frac{\epsilon_{cu}}{\epsilon_{cu} + 0.005}$, $\epsilon_t = \epsilon_{cu} * \frac{d_t - c}{c}$, and $d_t \approx d$

Eighth Step: select steel reinforcement

$$A_s = \rho b d$$

Ninth step: check strength of section

$$M_u \leq \varphi \rho b d^2 f_y \left(1 - 0.59 \rho \frac{f_y}{f'_c} \right)$$